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RSRE MEMORANDUM No. 4335

ROYAL SIGNALS & RADAR ESTABLISHMENT

SHORT RANGE, CLOSE TO GROUND, VHF/UHF PROPAGATION:
A COMPARISON OF MEASURED RESULTS WITH A
SIMPLE RAY-BASED MODEL

Author: P R Bellamy

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DATE:

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October 1989

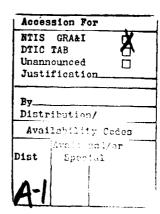
ABSTRACT

This report describes a VHF/UHF propagation prediction model and a series of field measurements aimed at verifying the results of the model. Comparisons between the model and the trial results were made at spot frequencies from 100 MHz to 900 MHz for several types of antenna and for various heights (not exceeding 2 metres) above ground level.

The predicted path losses from the model were found to agree quite well with the results of the field measurements. It should be noted that the prediction model was never intended to be a comprehensive tool, merely a utility package which could be incorporated into other software.

The program was written on an HP 9000 series model 310 computer using BASIC 5.1. This language has a set of commands which allow direct manipulation of complex values, consequently, translation into another language or version of BASIC not having these facilities will require extra programming.





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SHORT RANGE, CLOSE TO GROUND, VHF/UHF PROPAGATION: A COMPARISON OF MEASURED RESULTS WITH A SIMPLE RAY-BASED MODEL.

1. Introduction.

A requirement exists to study the propagation of signals between 100 MHz and 1GHz at ranges of less than 50m and with antenna heights less than 2m. A propagation loss prediction program was written employing geometric ray-theory which agreed quite closely with previously published data (Ref.1). However, this data did not include results obtained when one or both of the antennas is much less than 1m above the ground. It was therefore necessary to undertake a series of measurements using various types of antenna to validate predictions obtained from the model under the conditions for which no data was available.

This report describes both the propagation model and the trials devised to validate the predicted results.

2. Theoretical background to the prediction model.

Energy radiated from a transmitting antenna may be considered to consist of three parts - a direct wave which travels along a direct path from transmitting antenna to receiving antenna, an earth-reflected wave which arrives at the receiving antenna following a reflection at the earth's surface, and a surface wave which is supported by and travels along the earth's surface. The direct wave and the ground reflected wave (the sum of which is known as the space wave) can be accounted for by ray theory whereas the surface wave requires a solution of suitable electromagnetic field equations.

The propagation model calculates propagation loss between two similar antennas by evaluating the sum of the direct ray and the ground reflected ray at the receiving antenna. The effect of the surface wave is relatively small at frequencies above about 100 MHz and is omitted from the model (it does become more significant if the antennas heights are small in terms of wavelengths and if vertical rather than horizontal polarisation is used but in the present context the error is still small).

2.1 Ground reflection coefficient.

The electrical properties of the ground are represented by the following equation for refractive index (assuming $\epsilon_r = 1$, $\sigma = 0$, for air),

$$n = \sqrt{(\epsilon_r - j\frac{\sigma}{\omega \epsilon_0})}$$

where ϵ_{r} = ground relative permittivity

 σ - ground conductivity

 $\omega = 2\pi f$

 ϵ_{o} = permittivity of free space (8.854X10⁻¹² F/m)

 μ_r is taken as unity for both ground and air.

Typical values for the frequency range under consideration are:

For wet soil,
$$\epsilon_{r} = 15$$
 $\sigma = 0.1$

For dry soil,
$$\epsilon_{r} = 4$$
 $\sigma = 0.0001$

The following equations give the ground reflection coefficient in terms of n^2 (Ref.3) :

For vertical polarisation,

$$R = \frac{n^2 \sin \theta - \sqrt{(n^2 - \cos^2 \theta)}}{n^2 \sin \theta + \sqrt{(n^2 - \cos^2 \theta)}}$$

For horizontal polarisation,

$$R = \frac{\sin \theta - \sqrt{(n^2 - \cos^2 \theta)}}{\sin \theta + \sqrt{(n^2 - \cos^2 \theta)}}$$

where n^2 is defined above and θ is the angle of incidence between the ray and the horizontal.

If these functions are represented graphically it will be seen that for small angles of incidence the reflection coefficient for horizontal polarisation is approximately -1. With vertical polarisation |R| falls to a minimum at the Brewster angle and arg R changes from 180° to 0°. Appendix 4 gives some plots of the reflection coefficient for various types of reflecting surface.

The above formulae assume "smooth" reflecting surfaces. At the wavelengths under consideration most surfaces will appear smooth at small angles of incidence, but at larger angles diffraction effects will become apparent. These effects are not included in the propagation model.

2.2 Calculation of path loss.

The path loss between two antennas of gains \mathbf{g}_{T} and \mathbf{g}_{R} , at a frequency f and a distance d apart is given by,

L=10 log
$$g_T + 10 \log g_R + 10 \log (c^2/4\pi) - 20 \log (f) + 10 \log (1/4\pi d^2)$$

The last term is the free space loss, the remaining terms take account of the antenna gains and the aperture of the receiving antenna which, of course, is frequency dependent.

Fig. 2.1 illustrates the geometry of a typical multipath situation. If the contributions from the surface wave and any remote structures are ignored then the signal arriving at the receiving antenna is primarily composed of the direct ray and the ground reflected ray. The lengths of these paths are,

For the direct ray, $D = \sqrt{((h1-h2)^2 + d^2)}$ For the reflected ray, $R = \sqrt{((h1+h2)^2 + d^2)}$ and the grazing angle is,

$$\theta$$
 = arctan ($\frac{h1+h2}{d}$)

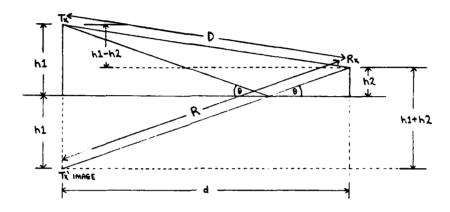


Fig. 2.1 Multipath geometry.

The propagation model uses these relationships to work out the relative amplitudes and phases of the direct and reflected rays at the receiving antenna. Remember that the phase angle between the rays is a combination of the path length difference and the phase change due to the reflection coefficient. The phasor sum of the two rays is plotted as site attenuation versus distance where site attenuation is defined as,

Site attenuation - Power transferred by direct connection Power transferred by propagation paths

Propagation prediction software.

A complete listing of the program is contained in Appendix 2. It is written in HP BASIC 5.1 and the COMPLEX binary must be resident. The user is prompted to enter frequency, range, antenna heights and gains, polarisation and the ground constants. Vertical scaling limits are set by the variables Ymax and Ymin and may be changed to suit a particular simulation.

Measurement of propagation loss.

4.1 Introduction.

The aim of the propagation measurement trial was primarily to validate the results produced by the propagation model. However, the choice of antenna types and the heights and distances involved was to a large extent determined by the application.

With reference to the definition of site attenuation given above it will be seen that a measurement of this quantity will require knowledge of the losses in the cables connecting the transmitter to the transmit antenna and the receive antenna to the receiver. This would be accomplished by connecting the cables directly together at the antennas and measuring the amount of power transferred at the frequency of interest. With the antennas reconnected and separated by a known distance a second measurement of transmitted power is made. The site attenuation is then the ratio of these two levels or in decibels,

Site attenuation = P1 - P2

where P1 = power received by direct connection (dB) P2 = power received via antennas (dB)

In practice, the measurement of Pl need only be performed once at each frequency of measurement and used for any subsequent antenna separation and/or antenna type.

4.2 <u>Description of equipment employed.</u>

Jaka Salas

The transmit antennas were in a fixed position mounted on a tripod (except for the log-periodic antenna which was clamped onto a wooden stake driven into the ground). The receive antennas were mounted on a trolley which was moved by a motorised pulley arrangement up to a maximum distance of 50 metres. A serrated disc attached to one of the trolley wheels interrupted a light beam which caused pulses to be sent along a cable to a counter circuit inside the equipment cabin where the measurement software converted the pulses into distance travelled in metres.

For convenience a large proportion of the measurement procedure was carried out under computer control. A Hewlett-Packard 9000/310 machine was used with dual 3 1/2 inch disc drives for storage of programs and data. The RF measurements were made using an HP8753A Network Analyser which has a maximum output level of +25dBm and a 100dB dynamic range. Since single frequency measurements were being made the analyser was set to zero span which enabled readings to be taken fast enough for the required spatial resolution. In order to ensure a good signal to noise ratio a 1 Watt amplifier module was used at the output port of the network analyser. A listing of the software used to control the measurements is presented in Appendix 3.

The distances between the cabin housing the measuring equipment and the antennas necessitated long lengths of coaxial feeder cable. The loss of 100m of UR43 at 1GHz is about 70dB which would make meaningful measurements impossible.

Therefore Heliax cable was used where possible and UR67 where insufficient lengths of Heliax were available.

The following table lists the various combinations of antennas used in the trial.

TRANSMIT ANTENNA	RECEIVE ANTENNA	FREO. RANGE (MHz)
Chase UHA 9105 (dipole, bicone)	Singer (dipole)	100,300,500,700,900
Chase UHA 9105 (dipole)	1/4 wave whip	400,600
CLP 5130-2 Log-periodic	CLP 5130-2 Log-periodic	100,300,500,700,900

The procedure for taking a typical measurement would be as follows;

- 1) Run measurement software.
- 2) Calibrate network analyser at the required frequency.
- 3) Measure cable losses at this frequency.
- 4) Set up required antennas.
- 5) Move trolley toward transmit antenna and stop at 2m distance.
- 6) Ensure distance counter has reset.
- 7) Start software taking readings.
- 8) Start trolley moving away from transmit antenna.
- 9) Stop trolley at 50m
- 10) Store data on disc.

4.3 Description of trial site.

All the propagation trials were carried out on the antennas field at RSRE South Site. This site was far from ideal being quite cluttered and not particularly flat. However, rather than use a more remote site with the attendant problems of transport, power and communication it was decided to tolerate the non-ideal conditions. Fig. 4.1 shows a plan of the site.

The measuring equipment was housed in a shielded cabin with mains power taken from a nearby 15A power point.

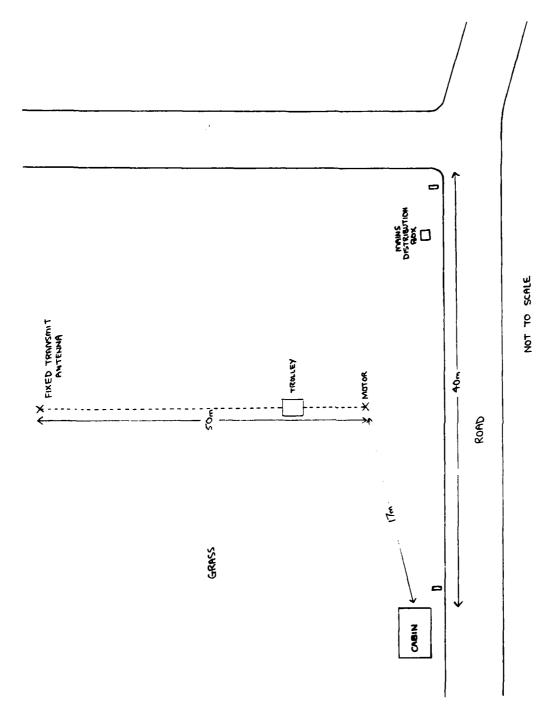


Fig. 4.1 Plan of trial site.

5. Results of the propagation measurement trial.

The results obtained from the trial are presented in a graphical format in Appendix 1. Each graph shows site attenuation in dB versus distance in metres both for the measured data and also the output of the prediction software. No measurement of the ground constants was undertaken and therefore typical values were used for the prediction. Small variations in the constants have little effect on the predicted results except to vary the sharpness of nulls.

The first set of measurements were intended to provide standard results against which the predictions of the propagation model could be compared. Half-wave dipoles were used for most measurements except at the lowest frequency (100 MHz) where a biconic antenna had to be used as the transmit antenna. Fig.Al.1 to Fig.Al.10 show the results of these measurements. In the prediction software the gains of the antennas were specified as 2.13dBi, the gain of a half-wave dipole relative to an isotrope.

The next set of measurements (Fig.Al.11 to Fig.Al.14) show the measured and predicted path losses between a dipole (1.7m) and a 1/4 wave vertically polarised whip close to ground level. In Fig.Al.11 the dipole was vertically polarised and the operating frequency was 400 MHz. In Fig.Al.12 the transmitting dipole was horizontally polarised and the whip vertically polarised but the simulation assumed both antennas horizontally polarised. This plot therefore gives some idea of the loss due to cross polarisation. Fig.Al.13 and Fig.Al.14 repeat these results but at 600 MHz.

The final measurements were performed using wide-band log-periodic antennas. Results were obtained every 200 MHz from 100 MHz to 900 MHz. The predicted results still assume dipole gains and so an indication of the gain of the log-periodic antennas can be obtained.

6. Discussion of trial results.

It can be seen by referring to the results in Appendix 1 that the measured and predicted results generally agree quite closely. However, there are some interesting discrepancies, most notably with regard to the position of the nulls. This is thought to be a consequence of the variation in height of the ground along which the trolley was moved, small changes in height can produce significant changes in null position. This error would also account for some of the discrepancy at longer ranges, for example in Fig.Al.1, if the nulls between 10m and 15m coincided then the error approaching 50m would not be so great. The position of the nulls is also affected by the angle of the ground reflection coefficient, but with horizontal polarisation the angle is almost always close to 180°. It is also possible that the surface wave changes null position but at frequencies greater than about 100 MHz the effect will be very small.

It is interesting to note that vertical polarisation suffers far less from deep nulls than horizontal. Appendix 4 shows that this is because the magnitude of the ground reflection coefficient is generally less with vertical polarisation than that with horizontal.

Discrepancies in the far field could in part be due to variation of the dipole gains with frequency. The predictions from the model assume constant gains of 2.13 dBi.

A further source of error will arise from the rather arbitrary choice of ground electrical parameters for the predicted results. Investigation of the effects of changing the ground parameters in the model has revealed that vertical polarisation at low frequencies is most sensitive in this respect. With horizontal polarisation, the most noticeable effect is on the depth of the nulls. These conclusions are in agreement with a similar investigation carried out in Ref.1.

Other possible sources of error are, reflections from nearby buildings and passing vehicles, signal cable leakage and additional radiation due to braid currents (imperfect balanced to unbalanced transformation).

7. Conclusions.

This report has presented the results of a comparison between measured propagation loss and predicted values from a simple computer model. Despite the simplicity of the model it has been shown to agree quite closely with the measured results. Furthermore, predictions from the model also tally with results from other models (Ref.1 and Ref.2).

It is intended to incorporate the model into other more complex simulations. This is relatively straightforward since the prediction program is quite short. Data generated by the package can be stored in arrays for further processing rather than being displayed directly.

Acknowledgements.

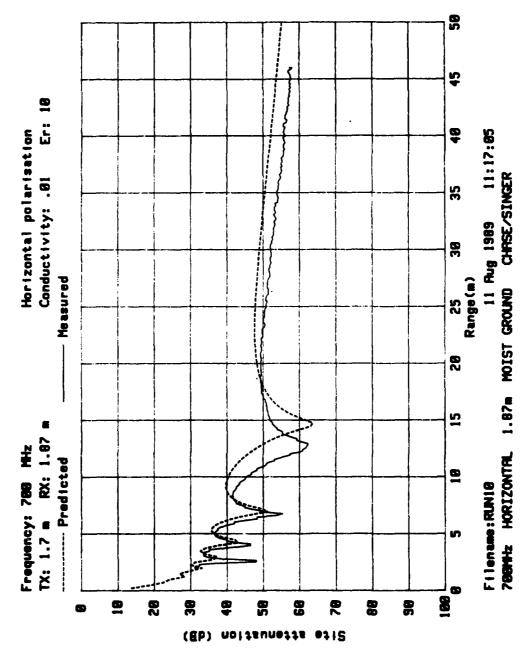
The author would like to thank A.W.Walker for his help in organising and running the propagation trial and especially with regard to setting up the trolley and motorised pulley system.

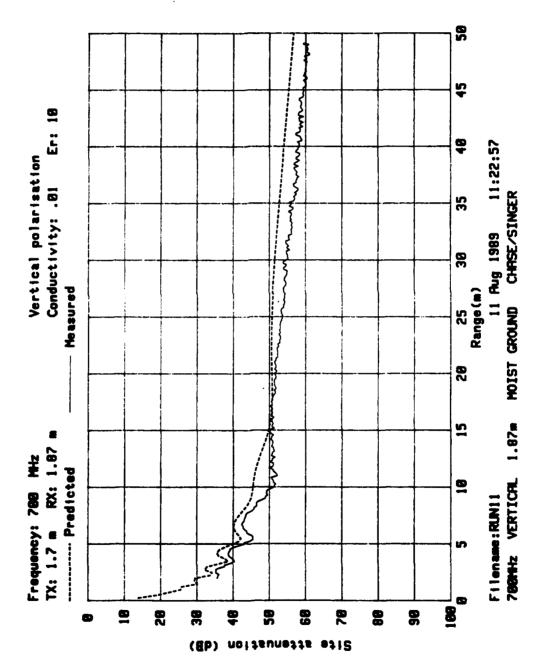
9. References.

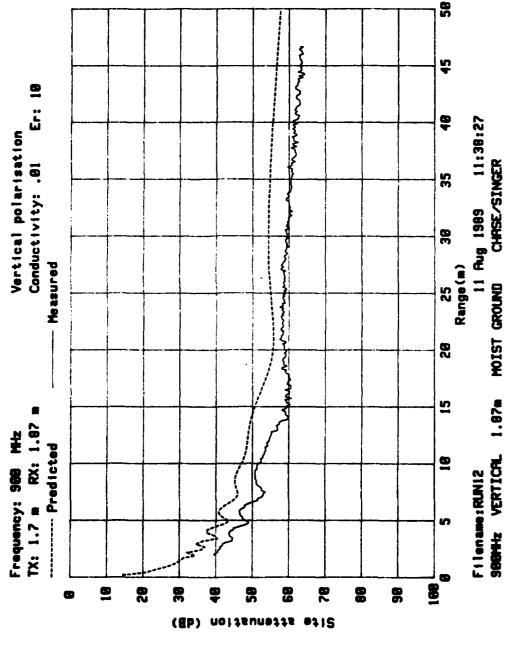
- 1. EDWARDS, J.A., BAGWELL, D.J., MEHLER, M.J., THOMAS, D., CHECKETTS, D.G., "Short Range V.H.F. Propagation", RSRE Research Contract Ref. ML32b/1557, Final Report September 1987.
- 2. WILKINSON, Dr.T.A., MATTHEWS, Prof.P.A., "Radio Communication Through Vegetation", MoD Agreement Ref. D/ER1/9/4/2062/138. Annual Report 21 July 1989.
- 3. REED, H.R., RUSSELL, C.M., "Ultra High Frequency Propagation", Wiley, Chapman & Hall, 1953, Chapter 4, pp 82 99, Chapter 5, pp 117 135

APPENDIX 1.

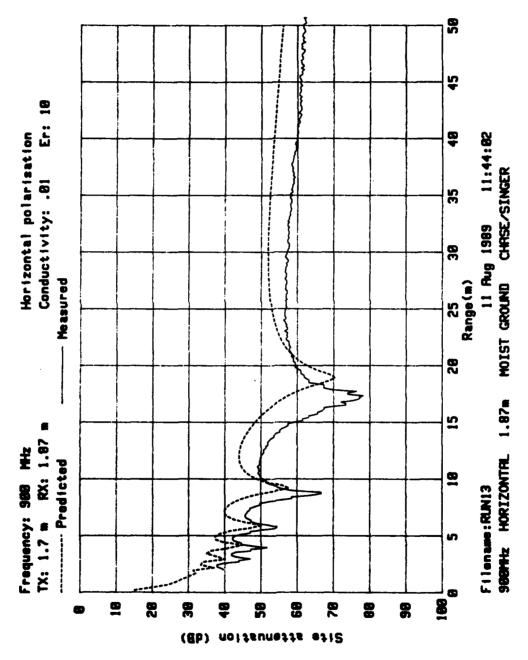
Results of propagation loss measurements.

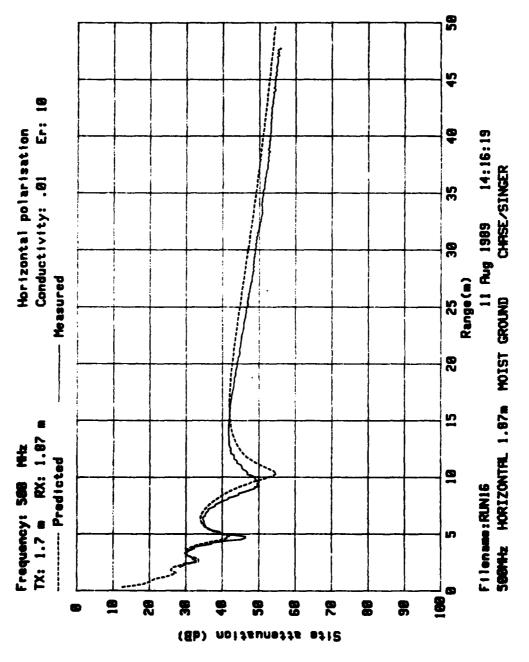


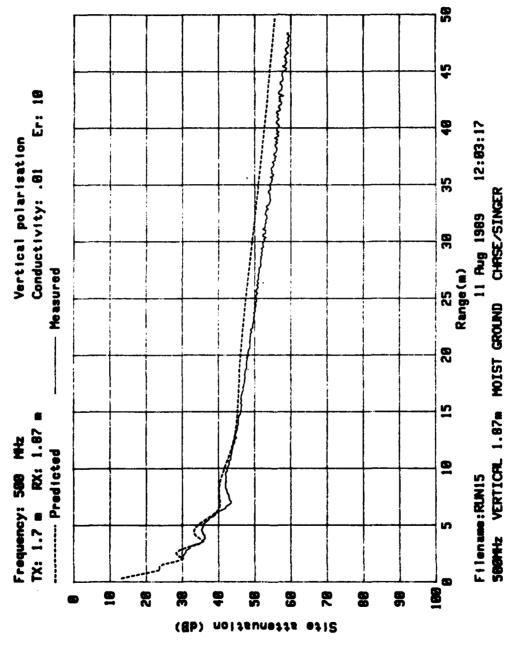


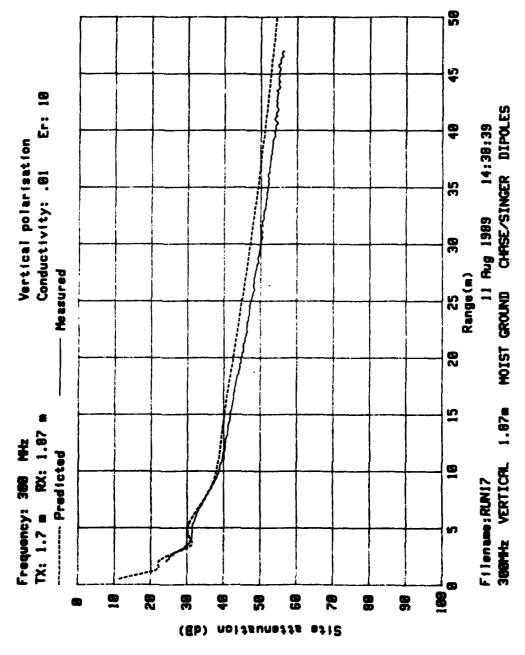


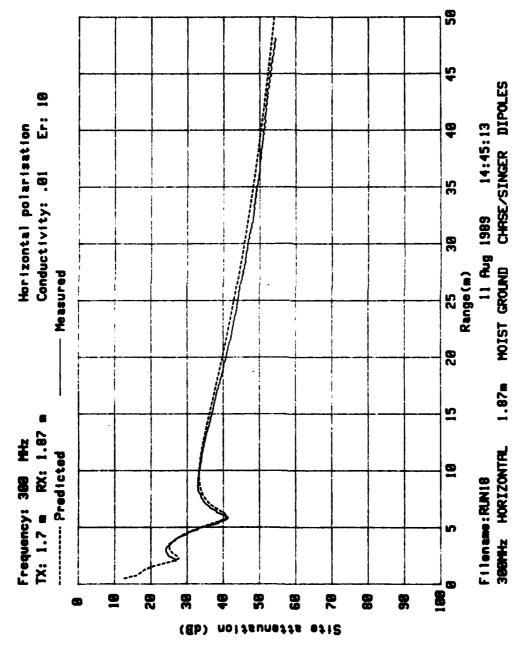
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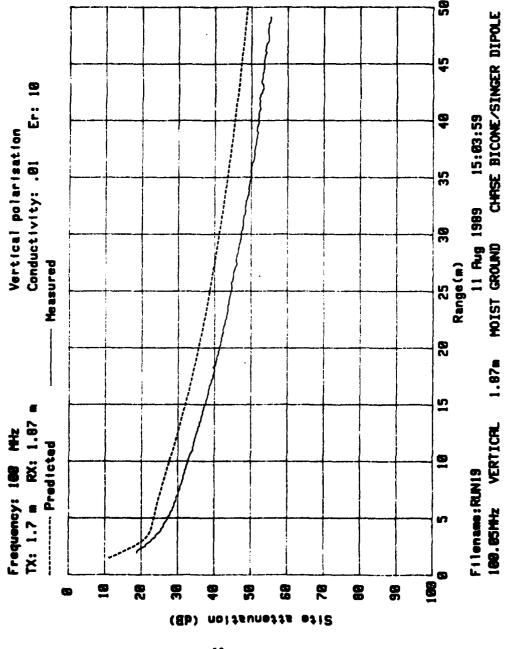


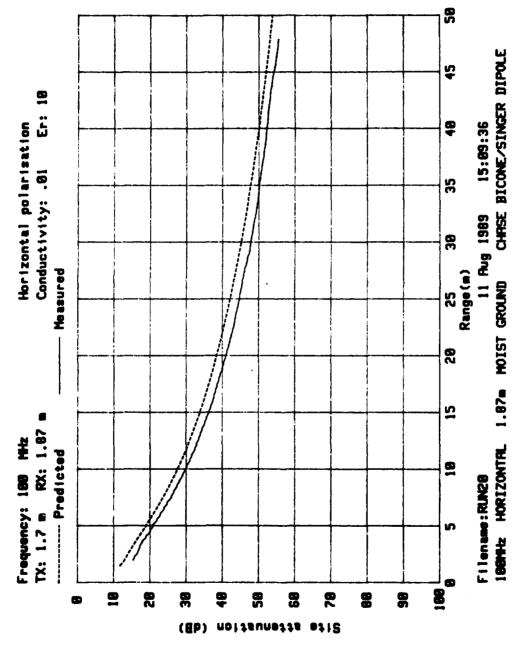


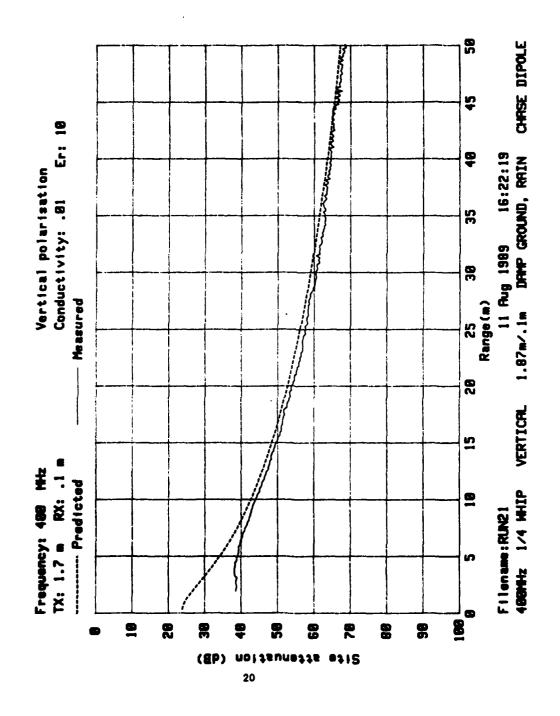




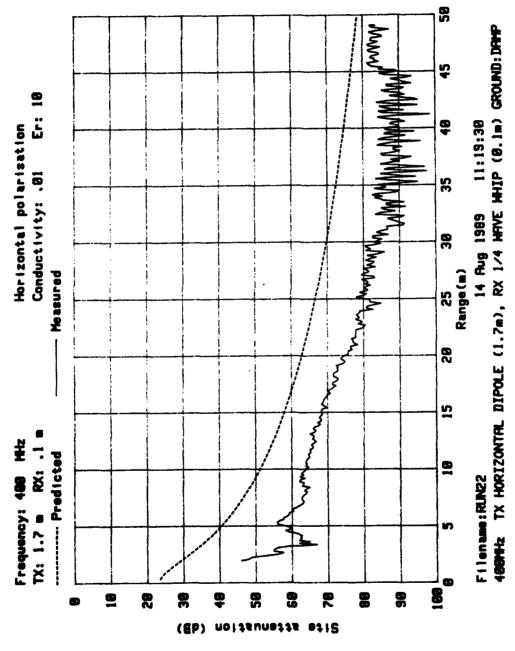


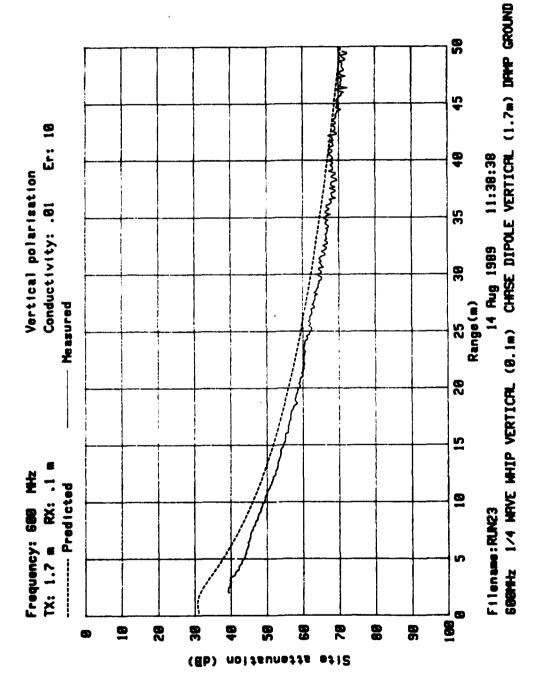


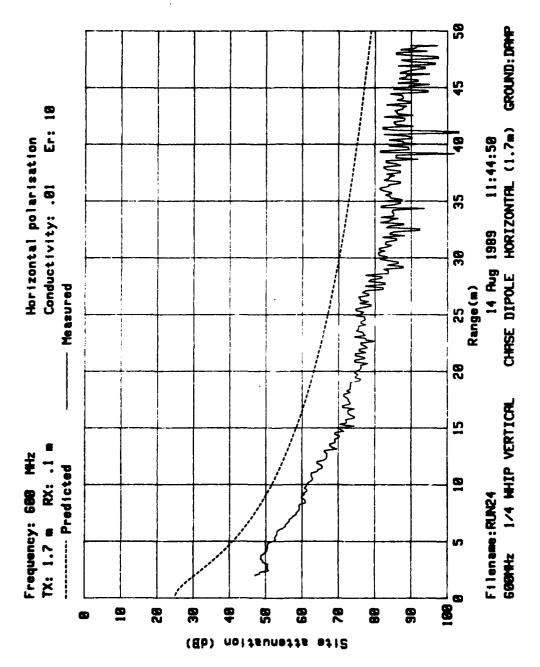


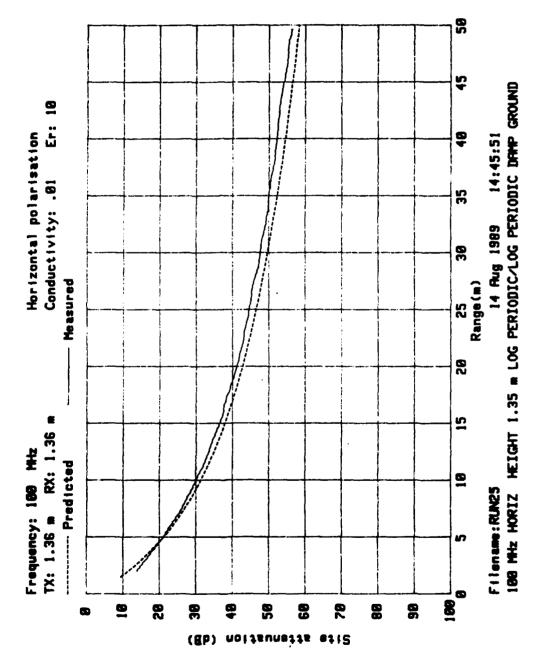


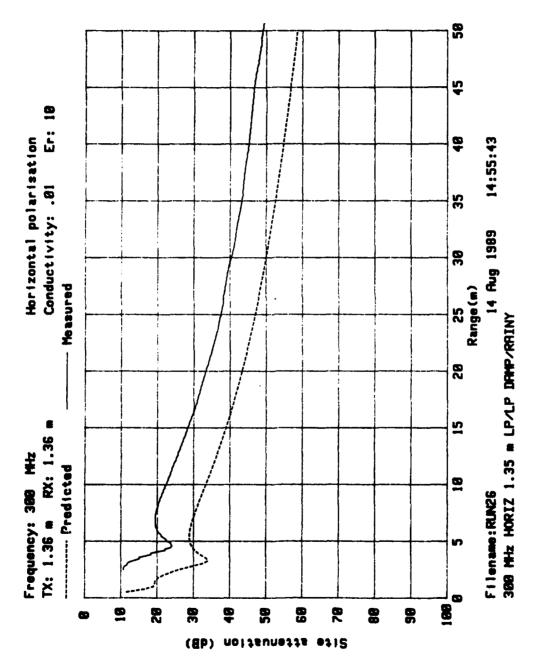
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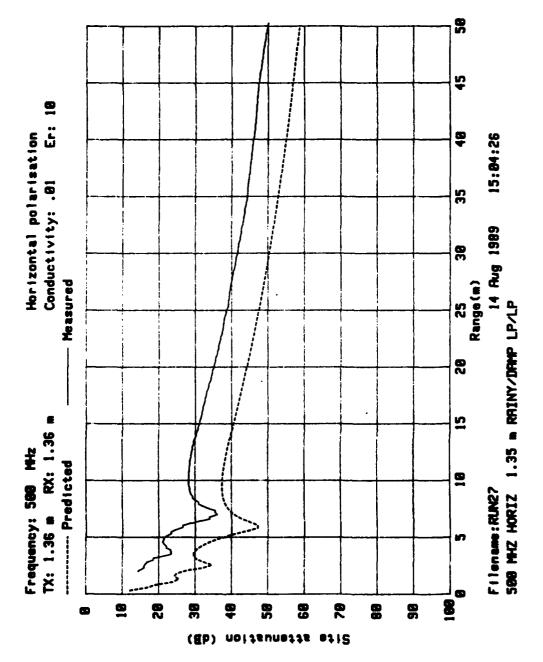




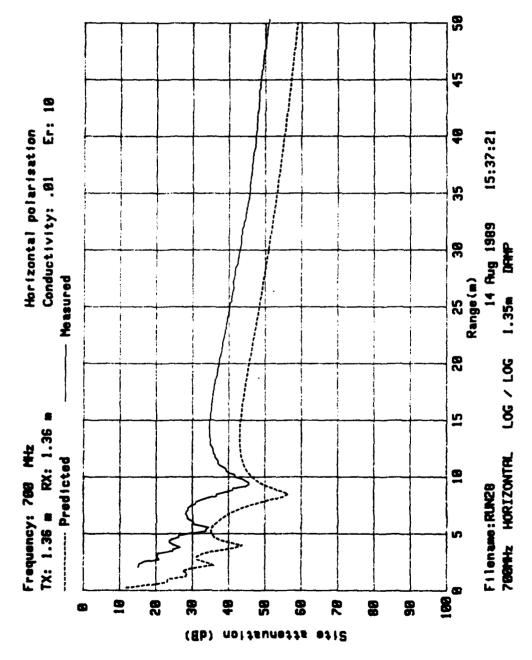


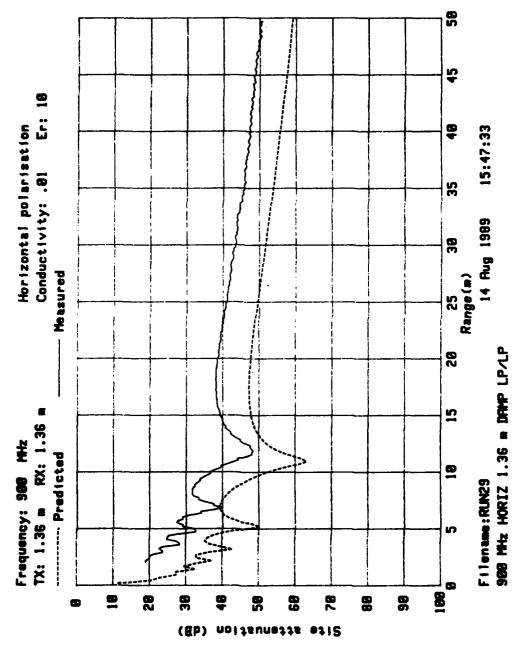


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APPENDIX 2.

Propagation prediction software

```
20 !
30 !
40 !
        SHORT RANGE VHF/UHF PROPAGATION PREDICTION PROGRAM
50 1
60 !
70 !
                                     May 1989
80 !
                      P.R.Bellamy
                                     VER 2 August 1989
90 1
100!
110!
        This software requires BASIC 5.1 with COMPLEX binary
120!
140
     COMPLEX N2,R,B,A
150
     REAL Free_space, Fresnel, D, Resultant, Freq, Range, H1, H2, Er, Sigma, Inc
     REAL Ymax, Ymin, L, C, EO, Lambda, Antenna_size, Antenna_factor, W, Topline, Nextlin
160
170
     REAL Graze, Theta, Angle, Ref_coeff, P1, P2, X, Y
180
     GINIT
190
     KEY LABELS OFF
200
     DEG
210
     CLEAR SCREEN
                    SHORT RANGE PROPAGATION MODEL
220
     PRINT "
     INPUT "FREQUENCY (MHz)?",Freq
INPUT "MAX. RANGE (m)?",Range
INPUT "TX ANTENNA HEIGHT (m)?",H1
230
240
250
     INPUT "RX ANTENNA HEIGHT (m)?", H2
260
     INPUT "TX ANTENNA GAIN (dBi)?",Gt
270
     INPUT "RX ANTENNA GAIN (dBi)?",Gr
INPUT "POLARISATION (H,V,Both)",Pol$
280
290
300
     INPUT "RELATIVE PERMITTIVITY?", Er
310
     INPUT "CONDUCTIVITY?", Sigma
320
     LINPUT "OUTPUT TO CRT OR PLOTTER?", Dev$
330
340
     IF Dev$[1]="P" OR Dev$[1]="p" THEN
350
       LINPUT "PLOTTER ADDRESS?", Add$
       PLOTTER IS VAL(Add$), "HPGL"
360
370
     ELSE
       PLOTTER IS CRT, "INTERNAL"
380
390
     END IF
                                     ! 300 HORIZONTAL POINTS
400
     Inc-Range/300
410
420
430
440
     Ymax-100
450
     Ymin-0
460
     VIEWPORT 10,120,7,85
470
     PEN 1
     WINDOW O, Range, Ymax, Ymin
480
490
     GRID Range/10,10,0,Ymax
500
     CLIP OFF
510
     CSIZE 3..5
520
     MOVE Range/2, Ymax+.07*(Ymax-Ymin)
530
     LORG 5
540
    LABEL "Range(m)"
```

```
550
      FOR L-0 TO Range STEP Range/10
       MOVE L, Ymax+.03*(Ymax-Ymin)
560
570
        LABEL L
580
      NEXT L
590
      MOVE -.08*Range, Ymax-(Ymax-Ymin)/2
600
      LDIR 90
      LABEL "Site attenuation (dB)"
610
620
      LDIR 0
      FOR L-Ymin TO Ymax STEP 10
630
        MOVE -. 03*Range, L
640
650
        LABEL L
660
      NEXT L
670
680
690
700
710
720
                         SPEED OF LIGHT
      C=3.E+8
730
      E0-8.854E-12
740
      Lambda=300/Freq
      Antenna_size=Lambda/2! ROUGH SIZE OF AERIAL
750
760
      Fresnel-2*Antenna_size*Antenna_size/Lambda! NEAR FIELD / FAR FIELD
770
      W=2*PI*Freq*1.E+6
780
      Antenna factor=Gt+Gr+10*LGT(C*C/(4*PI))-20*LGT(Freq*1.E+6)
790
800
810
      Topline=Ymin-.l*(Ymax-Ymin)
820
      Nextline=Ymin-.05*(Ymax-Ymin)
830
840
      LORG 2
850
      MOVE 0, Topline
860
      LABEL "Frequency: "; Freq; " MHz"
870
880
800
      MOVE Range/2, Topline
900
      IF Pol$="H" THEN LABEL "Horizontal"
      IF Pol$="V" THEN LABEL "Vertical"
910
920
      IF Pol$-"B" THEN
        PEN 2
930
940
        MOVE Range/2, Topline
950
        DRAW Range/1.8, Topline
960
        PENUP
970
        PEN 1
        LABEL " Horizontal"
980
990
        MOVE Range/1.4, Topline
1000
        PEN 3
1010
        DRAW Range/1.3, Topline
1020
        PENUP
        PEN 1
1030
        LABEL " Vertical"
1040
1050 END IF
1060 !
1070
1080 MOVE O Nextline
1090 LABEL "TX :";H1;"m RX :";H2;"m"
1100 MOVE Range/2, Nextline
1110 LABEL "Conductivity:"; Sigma;"
                                      Er:";Er
1120 !
```

```
1130 !
1140
1150 Next pol:IF Pol$-"V" THEN
1160
      PEN 3
1170
     ELSE
1180
       PEN 2
1190
     END IF
1200
1210
     FOR D-Fresnel TO Range STEP Inc
       P1-SQR((H1-H2)*(H1-H2)+D*D)
                                ! DIRECT PATH LENGTH
1220
1230
       P2-SQR((H1+H2)*(H1+H2)+D*D)
                                ! REFLECTED PATH LENGTH
                                   GRAZING ANGLE IN DEGREES
1240
       Graze-ATN((H1+H2)/D)
                          t
1250
       Theta=360*((P2-P1)/Lambda-INT((P2-P1)/Lambda))! PATH DIFFERENCE IN
1260
                                              DEGREES (i.e. PHASE)
1270
1280
1290
     <u>|</u>
1300
          CALCULATE REFLECTION COEFFICIENT
     | ***********************
1310
       N2-CMPLX(Er,-Sigma/(W*E0))
1320
1330
       B-SQR(N2-COS(Graze)*COS(Graze))
1340
       A-SIN(Graze)
1350
       IF Pol$-"V" THEN
1360
        R=(N2*A-B)/(N2*A+B)
1370
       ELSE
1380
        R=(A-B)/(B+A)
1390
       END IF
1400
       Ref_coeff=ABS(R)
1410
       Angle-ARG(R)
     ******************************
1420
1430
1440
1450
     ! ADD PHASORS.....
1460
       Free_space_d=SQR(30/(P1*P1))! FREE SPACE LOSS: DIRECT RAY
1470
       Free space_r=SQR(30/(P2*P2))! FREE SPACE LOSS: REFLECTED RAY
1480
       X-Free_space_d+Free_space_r*Ref_coeff*COS(Theta+Angle)
1490
       Y-Free space r*Ref coeff*SIN(Theta+Angle)
1500
      Resultant=(X*X+Y*Y)/(120*PI)
1510
1520
1530
1540
       1550
         PLOT THE RESULT..
1560
       PLOT D, -10*LGT(Resultant)-Antenna_factor
1570
       1580
1590
1600
     NEXT D
     IF Pol$-"B" THEN
1610
1620
      Po1$-"V"
1630
      PENUP
1640
      GOTO Next_pol
1650 END IF
1660
1670
1680 PENUP
1690
1700
    END
```

1710 !				
1720 !				
1730 !				
1740 !				
1750 !**	******	*******	*****	r**
1760 !	TYPICAL	. GROUND CONSTANTS		
1770 !				
1780 !		SIGMA (Mhos/M)	EPSILON	
1790 !	Sea water	5	80	
1800 !	Fresh water	8e-3	80	
1810 !	Dry sandy coastal	2e-3	10	
1820 !	Marshy forested	8e-3	12	
1830 !	Rich agricultural	1e-2	15	
1840 !	Pastoral rolling	5e-3	13	
1850 !	Rocky, mountainous	2e-3	5	
1860 !	Mountainous	le-3	5	
1870 !	Cities, residential	2e-3	5	
1880 !	Cities, industrial	1e-4	3	
1890 !				
1900 !				
1910 1				

APPENDIX 3.

Trial control software

```
10
    20
30
         SHORT RANGE PROPAGATION
                                           TRIAL
40
50
                      CONTROL SOFTWARE
51
52
             (c) P.R.Bellamy / I.R.Dixon
                                   1 Aug 1989
53
70
    80
81 Start:
90
    OPTION BASE 1
100
110
    120
                     Variable declarations
130
    140
    DIM Message$[40], Answer$[1], File$[10], K$[1]
150
    REAL Prop_data(32767,2)
160
    INTEGER Big_cog_teeth, Lit_cog_teeth, Max_readings, Max_distance, Pulse_per_re
v, Net_an, Gpio, Readings
170
    INTEGER Cal_done, True, False, Wanted_freq
    REAL Freq, Dist_per_pulse, Gear_ratio, Wheel_circum, Max_dist_pulse, Null
180
190
200
    210
220
                    MAIN
                            PROGRAM
    230
231
    GOSUB Initial_values
240
241
250
    Input freq(Freq)
251
260
    Set_up_8753(Freq)
262
270
    Calibrate_8753
271
280
    Check_freq(Freq, Wanted_freq)
281
    IF NOT Wanted freq THEN
     Entry_beep
DISP "CONTINUE WITH ";Freq;" MHz (y)?"
282
284
     Wait_key(K$)
285
286
     IF K$◇"Y" AND K$◇"y" THEN GOTO Start
287
    END IF
288
290
   Reset_counter(Gpio)
291
300
    GOSUB Take_readings
301
303
   !GOSUB Test_data
304
306
    KEY LABELS OFF
307
    REDIM Prop_data(Readings-1,2)
308
310
    Plot_data(Prop_data(*),Dist_per_pulse)
311
```

DISP "Store data on disc? (n)"

```
Entry_beep
Wait_key(K$)
313
315
316
     IF K$-"N" OR K$-"n" THEN
       DISP "NO! ARE YOU ABSOLUTELY SURE?"
317
318
       Entry beep
       Wait_key(K$)
IF K$-"Y" OR K$-"y" THEN
320
321
322
        CLEAR SCREEN
        PRINT "PROGRAM TERMINATED"
323
324
        PAUSE
       END IF
325
326
     END IF
327
328
     Store_data(Prop_data(*))
329
330
     CLEAR SCREEN
331
     DISP "FINISHED."
     *****************
333
334
     STOP
335
340 Initial values: !
350
     PRINTER IS CRT
360
     CLEAR SCREEN
370
     KEY LABELS OFF
                                 SHORT RANGE PROPAGAT
380
    PRINT CHR$(140); CHR$(132);"
ION TRIAL
                            ";CHR$(136);CHR$(128)
390 PRINT "
           Initialising variables....";
400
     GINIT
     Max_readings=5000
                                       !Max number of readings (<32768)
410
     Max_distance=100
                                       !Distance in metres
420
430
440
     Wheel circum-.776
450
     Big_cog_teeth=162
     Lit_cog_teeth=20
460
470
     Gear_ratio=Big_cog_teeth/Lit_cog_teeth
480
     Pulse_per_rev=100
490
     Dist_per_pulse=Wheel_circum/(Gear_ratio*Pulse_per_rev)
500
     Max_dist_pulse=INT(Max_distance/Dist_per_pulse)-32768
510
520
     Net_an=716
530
     Gpio-12
540
550
     White-1
560
     Red-2
570
     Yellow-3
580
     Green-4
590
     Cyan-5
600
     Blue-6
610
     Magenta-7
620
     PRINT "done."
630
640
     RETURN
650
660
670 Take_readings: !
680
    CLEAR SCREEN
```

```
PRINT "
                         DATA
                                  GATHERING
                                                        ROUTINE"
681
682
     KEY LABELS ON
683
      CONTROL 2,2;1
     ON KEY 1 LABEL " ABORT" GOTO Abort
684
686
     PRINT "
              PRESS KEY 1 TO ABORT MEASUREMENT"
687
688
     Readings-1
689
     Entry beep
DISP *PRESS RETURN TO START MEASUREMENT...*
691
     Wait_key(K$)
692
693
     DISP TAKING DATA....
694
     REPEAT
       OUTPUT Net_an; "OUTPMARK; "
695
696
       ENTER Net_an; Prop_data(Readings, 2), Null, Null
697
       CONTROL Gpio,2;0
698
       STATUS Gpio, 3; Prop_data(Readings, 1)
699
       CONTROL Gpio,2;1
700
       Readings-Readings+1
701
     UNTIL Readings>Max_readings
702
     Err(3)
703
     RETURN
704 Abort: !
705
     Err(2)
706
     RETURN
920
921
922 Test_data: !
930 CLEAR SCREEN
                         DATA GATHERING ROUTINE"
931
     PRINT "
932
     PRINT "
            WARNING: THIS ROUTINE DOES NOT READ THE DISTANCE COUNTER"
934
     KEY LABELS ON
935
     CONTROL 2,2;1
936
     ON KEY 1 LABEL " ABORT" GOTO Abort2
937
     PRINT "
             PRESS KEY 1 TO ABORT MEASUREMENT"
938
939
     Readings-1
     Entry beep
DISP **PRESS RETURN TO START MEASUREMENT...*
940
942
943
     Wait_key(K$)
944
     DISP "TAKING DATA....
945
     TO-TIMEDATE
946
     REPEAT
       OUTPUT Net_an; "OUTPMARK; "
947
948
       ENTER Net_an; Prop_data(Readings, 2), Null, Null
949
       Prop_data(Readings,1)=Readings*30.0
950
       Readings-Readings+1
     UNTIL Readings>Max_readings
951
952
     Err(3)
```

```
953 RETURN
954 Abort2: 1
955
     T1-TIMEDATE
956
     PRINT "TIME PER READING: "; (T1-T0)/Readings; " SECS"
957
     Err(2)
958
     RETURN
959
960
961
962
     END
963
964
                  SUBPROGRAM DEFINITIONS
965 Set_up_8753: !
     SUB Set_up_8753(REAL Freq)
966
       Na-716
967
968
        ABORT 7
969
        OUTPUT Na; "PRES; "
                                            PRESET 8753
970
       OUTPUT Na; "FORM3; POIN 3; "
                                            !FORMAT 3, 3 POINTS
971
       OUTPUT Na; "LOGM; "
                                            !LOG MAG DISPLAY
        OUTPUT Na; "CHAN1; "
972
                                            !CHANNEL 1 ACTIVE
975
       OUTPUT Na; "IFBW30; "
                                           !IF BANDWIDTH
       OUTPUT Na; "POWE 0;"
976
                                            !SOURCE POWER
977
       OUTPUT Na: "S21:"
                                            !TRANSMISSION MEASUREMENT
       OUTPUT Na; "CENT "; Freq; " MHZ; SPAN O MHZ; " !SET CENTRE FREQ AND SPAN
978
979
980
       A$-CHR$(34)&"PROPCAL"&CHR$(34)
                                            !TITLE REG 5
981
        OUTPUT Na; "TITR5; "&A$&"; "
982
     SUBEND
983
984
985 Calibrate_8753: !
986
     SUB Calibrate 8753
987
       CLEAR SCREEN
988
       PRINT "
                                      8 7 5 3
                                                CALIBRATION
       PRINT "
989
```

```
990
        Entry_beep
991
        INPUT "LOAD CAL DATA FROM 8753 REG 5? (Y/N)".Reply$
992
        IF Reply$-"Y" OR Reply$-"y" THEN
          OUTPUT 716; "OPC?; RECA5; "
993
994
          ENTER 716; Reply
995
        ELSE
996
          OUTPUT 716; "CALKN50; "
          OUTPUT 716; "CALIFUL2;"
997
                                              !FULL 2 PORT CALIBRATION
998
          OUTPUT 716; "REFL;"
999
          DISP "CONNECT OPEN TO PORT 1 THEN PRESS RETURN..."
1000
1001
          CALL Wait_key(K$)
          OUTPUT 716; "CLASS11A; OPC?; STANB; "
1002
1003
          ENTER 716; Reply
1004
1005
          DISP "CONNECT SHORT TO PORT 1 THEN PRESS RETURN..."
```

```
1006
          CALL Wait_key(K$)
1007
          OUTPUT 716; "CLASS11B; OPC?; STANB; "
1008
          ENTER 716; Reply
1009
1010
          DISP "CONNECT LOAD TO PORT 1 THEN PRESS RETURN..."
          CALL Wait_key(K$)
1011
1012
          OUTPUT 716; "CLASS11C; OPC?; STANA; "
          ENTER 716; Reply
1013
1014
          DISP "CONNECT OPEN TO PORT 2 THEN PRESS RETURN..."
1015
1016
          CALL Wait_key(K$)
1017
          OUTPUT 716; "CLASS22A; OPC?; STANB; "
1018
          ENTER 716; Reply
1019
          DISP "CONNECT SHORT TO PORT 2 THEN PRESS RETURN..."
1020
1021
          CALL Wait key(K$)
          OUTPUT 716; "CLASS22B; OPC?; STANB; "
1022
1023
          ENTER 716; Reply
1024
          DISP "CONNECT LOAD TO PORT 2 THEN PRESS RETURN..."
1025
1026
          CALL Wait key(K$)
          OUTPUT 716; "CLASS22C; OPC?; STANA; "
1027
1028
          ENTER 716; Reply
1029
          OUTPUT 716; "REFD;"
1030
1031
          DISP "CONNECT THRU THEN PRESS RETURN..."
1032
1033
          CALL Wait_key(K$)
          OUTPUT 716; "TRAN;"
1034
1035
          OUTPUT 716; "OPC?; FWDT; "
1036
1037
          ENTER 716; Reply
1038
1039
          OUTPUT 716; "OPC?; REVT; "
1040
          ENTER 716; Reply
1041
1042
          OUTPUT 716; "OPC?; FWDM; "
1043
          ENTER 716; Reply
1044
1045
          OUTPUT 716; "OPC?; REVM; "
          ENTER 716; Reply
1046
          OUTPUT 716; "TRAD;"
1047
1048
1049
          OUTPUT 716; "ISOL; "
1050
          OUTPUT 716: "OMII: "
          OUTPUT 716; "ISOD; "
1051
1052
          OUTPUT 716; "SAV2;"
1053
1054
          OUTPUT 716; "OPC?; SAVE5; "
          ENTER 716; Reply
1055
1056
          Cal done-True
1057
        END IF
1058
        DISP "CALIBRATION COMPLETE"
1059
        WAIT 1
1060
        CLEAR SCREEN
1061 SUBEND
1062
1063 !
```

```
1064 Wait_key: !
1065 SUB Wait_key(K$)
1066
        DIM TS[10]
        ON KBD GOTO Quit
1067
1068
        LOOP
1069
         END LOOP
1070 Quit: !
        T$-KBD$
1071
1072
         K$-T$[1,1]
1073
      SUBEND
1074
1075 !
1076 Input_freq: !
1077 SUB Input freq(REAL Freq)
1078
         Entry_beep
1079
         LOOP
         INPUT "Frequency for this measurement (MHz) ",Freq EXIT IF NOT (Freq<100) AND NOT (Freq>1000)
1080
1081
1082
          Err(1)
1083
         END LOOP
1084
      SUBEND
1085
1086
1087 Err: !
                MASTER ERROR HANDLING ROUTINE
1088 SUB Err(INTEGER Err num)
1089
         SELECT Err_num
1090 !
1091
         CASE 1
1092
           DISP "FREQUENCY OUT OF RANGE";
1093
1094
         CASE 2
1095
          DISP "MEASUREMENT ABORTED";
1096
1097
         CASE 3
           DISP "MAXIMUM NUMBER OF READINGS EXCEEDED";
1098
1099
1100
         CASE 4
           DISP "CALIBRATION DATA NOT VALID AT THIS FREQUENCY";
1101
1102 !
1103
1104
           DISP "RESET FAILED"
1106
1107
         CASE ELSE
1108
         END SELECT
         DISP " <SPACE> TO CONT"
1109
1110
         BEEP 1000,.2
1111
         Wait_key(K$)
1112
         DISP
1113 SUBEND
1114 !
1115 !
1116 Entry_beep: !
1117 SUB Entry_beep
1118
        BEEP 900,.05
1119 SUBEND
1120
1121 !
1122 Reset_counter: !
```

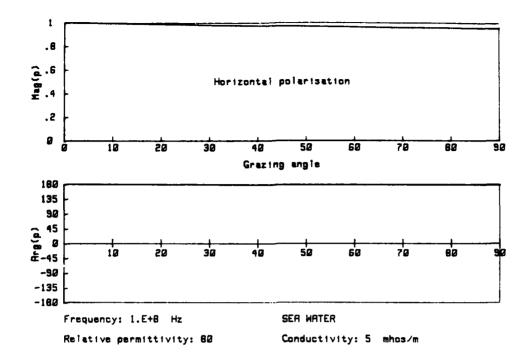
```
1123 SUB Reset_counter(INTEGER Gpio)
1124
        INTEGER A
      ! Outputs a reset pulse to the distance counter on CTL1
1125
1126 Do_again: !
1128
         CONTROL Gpio,2;1: CTL1-1 (RESET HIGH), CTL0-0 (CONTROL LOW)
1129
        WAIT .1
1130
        CONTROL Gpio,2;3! CTL1-0 (RESET LOW ), CTL0-0 (CONTROL LOW)
1131
        WAIT .1
        CONTROL Gpio,2;1! CTL1-1 (RESET HIGH), CTL0-0 (CONTROL LOW)
1132
1133
1134
        DISP "RESET PULSE SENT - MOVE WHEEL THEN PRESS A KEY.."
1135
        Wait_key(A$)
1137
        CONTROL Gpio, 2;0
1138
        STATUS Gpio, 3; A
1139
        CONTROL Gpio, 2;1
1140
        IF A<0 OR A>100 THEN
1141
          Err(5)
1142
          GOTO Do_again
1143
        END IF
1144
      SUBEND
1145 !
1146 1
1147 Check freq: !
1148 SUB Check_freq(REAL Freq, INTEGER Flag)
1149
        REAL F
1150
        Flag-1
        OUTPUT 716; "CENT?;"
1151
1152
        ENTER 716; F
1153
        IF F⇔Freq*1.E+6 THEN
1154
          CALL Err(4)
1155
          Freq-F/1.E+6
1156
          Flag-0
1157
        END IF
1158 SUBEND
1159 !
1160 !
1161 Plot_data: !
1162 SUB_Plot_data(REAL_Prop_data(*),Dist_per_pulse)
        INTEGER White, Red, Yellow, Green, Cyan, Blue, Magenta
1163
1164
        INTEGER I
1165
        White-1
1166
        Red-2
        Yellow-3
1167
1168
        Green-4
1169
        Cyan-5
1170
        Blue-6
1171
        Magenta-7
1172
1173
        CLEAR SCREEN
1174
        GINIT
1175
        GCLEAR
1176
        GRAPHICS ON
1177
        INPUT "Start distance:",Start_pos
        INPUT "Amp gain (dB): ", Gain
1178
1179
        PEN White
1180
        Readings-SIZE(Prop_data, 1)
1181 !
1182
        VIEWPORT 10,120,28,95
```

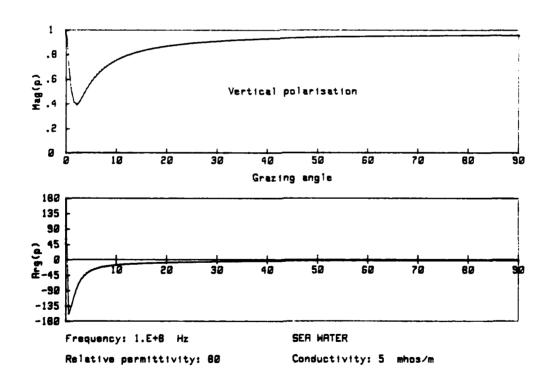
```
WINDOW 0,50,100,0
1183
1184
        AREA PEN Blue
1185
        MOVE 0.0
        RECTANGLE 50,100, FILL
1186
        AXES 1,2,0,100,10,5,3
1187
1188
1189
        CLIP OFF
        CSIZE 2.5
1190
1191
        LDIR 0
1192
        LORG 8
        FOR I-0 TO 100 STEP 10
1193
          MOVE 0, I
1194
1195
          LABEL I
1196
        NEXT I
        CSIZE 3
1197
1198
        LORG 4
1199
        LDIR 90
1200
        MOVE -3,50
        LABEL "Site attenuation (dB)"
1201
1202
1203
        CSIZE 2.5
        LDIR 0
1204
1205
        LORG 6
1206
        FOR I=0 TO 50 STEP 10
1207
          MOVE 1,100
1208
          LABEL I
1209
        NEXT I
1210
        CSIZE 3
1211
        MOVE 25,102
1212
        LABEL "Range (m)"
1213
1214
        MOVE 40,0
1215
        LDIR 0
        LORG 4
1216
1217
        CSIZE 2.7
1218
        LABEL DATE$(TIMEDATE); " "; TIME$(TIMEDATE)
1219
1220
        FOR 1-2 TO Readings
1221
          Dist=FNDistance(Prop_data(I,1),Dist_per_pulse)+Start_pos
1222
          Prop_data(I,2)=-Prop_data(I,2)+Gain
1223
          PLOT Dist, Prop_data(I,2)
1224
          Prop_data(I,1)=Dist
1225
        NEXT I
1226
      SUBEND
1227
1228 1
1229 !
1230 DEF FNDistance(REAL Counter, Dist_per_pulse)
1231
        IF Counter<0 THEN
          RETURN (Counter+65536)*Dist_per_pulse
1232
        ELSE
1233
          RETURN Counter*Dist_per_pulse
1234
1235
        END IF
1236 FNEND
1237
1238
     •
1239 Store_data: !
                 ! Creates file on which the data in Prop_data is stored
1240
```

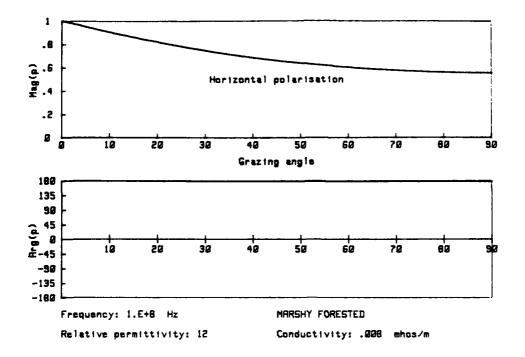
```
! Summary$ is a 160 character (2 line) summary
1241
1242 SUB Store_data(REAL Prop_data(*))
1243 ON ERROR GOTO Trap
1244
        CLEAR SCREEN
1245
        DIM Summary$[160]
1246
        DIM FileS[25]
        Readings-SIZE(Prop_data,1)
1247
1248
1249
        PRINT TABXY(1,21); "SUMMARY: (2 lines max)"
1250
        LINPUT Summary$
1251
1252 Inp:LINFUT "File:mass storage unit?", File$
1253
        DISP "Creating file..."
                                                        ! NOTE: BASIC 5 seems to w
        CREATE BDAT File$, Readings *16+500,1
1254
ork out
                                                    the correct file size itself!
1255
                                         1
1256
        ASSIGN @Path TO File$
        DISP "Storing data . . . "
1257
        OUTPUT @Path; Summary$, TIMEDATE, Readings, Prop_data(*)
1258
1259
        ASSIGN @Path TO *
1260
        DISP "
        SUBEXIT
1261
1262
1263 Trap: !
        DISP ERRM$;" <SPACE> TO CONT"
BEEP 1000,.2
1264
1265
1266
        Wait_key(K$)
        GOTO Inp
1267
1268 SUBEND
```

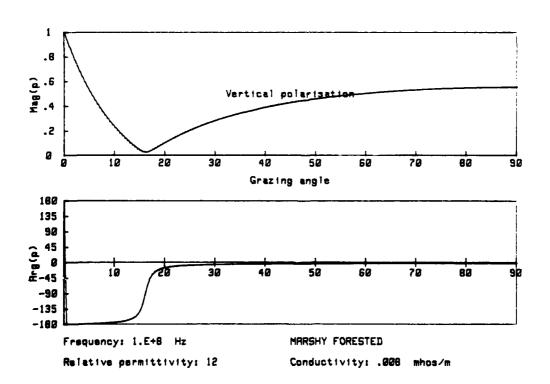
APPENDIX 4.

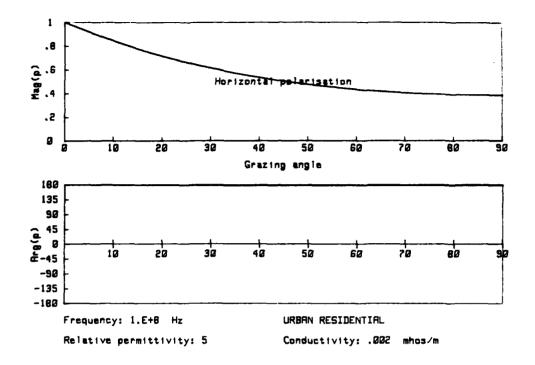
Ground reflection coefficient plots

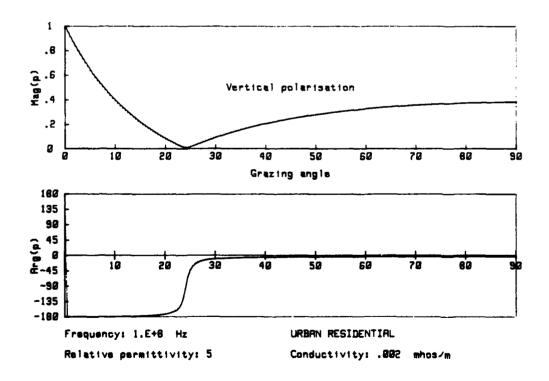












DOCUMENT CONTROL SHEET

1. DRIC Reference (if known)	2. Originator's Refer	rence 3. Agency Reference	4. Report Sec U/C C	urity lassification
5. Originator's Code (if known) 7784000	ROYAL SIGNALS	rate Author) Name and Locations and Radar Establish Dad, Great Malvern, RE WR14 3PS		
5a. Sponsoring Agency's Code (if known)	6a. Sponsoring Agency	y (Contract Authority) Name	and Location	
7. Title SHORT RANGE,	CLOSE TO GROUND,	VHF/UHF PROPAGATION		
7a. Title in Foreign Language	(in the case of trans)	lations}		
7a. Title in Foreign Language	(in the case of trans)	lations}		
7a. Title in Foreign Language 7b. Presented at (for conferen				
	nce napers) Title, pl		10. Date 1989.10	pp. ref. 47
7b. Presented at (for conferent 8. Author 1 Surname, initials BELLAMY P R	nce napers) Title, pl	lace and date of conference		47
7b. Presented at (for conference of the conferen	nce napers) Title, pl	9(b) Authors 3,4	1989.10	47
7b. Presented at (for conferent 8. Author 1 Surname, initials BELLAMY P R 11. Contract Number 15. Distribution statement	nce napers) Title, pl	9(b) Authors 3,4	1989.10	47
7b. Presented at (for conferent 8. Author 1 Surname, initials BELLAMY P R 11. Contract Number 15. Distribution statement UNLIMITED	nce napers) Title, pl	9(b) Authors 3,4	1989.10	47
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7b. Presented at (for conferent 8. Author 1 Surname, initials BELLAMY P R 11. Contract Number 15. Distribution statement UNLIMITED Descriptors (or keywords)	9(a) Author 2	9(b) Authors 3,4 13. Project continue on separate	1989.10 14. Other Re	47
7b. Presented at (for conferent 8. Author 1 Surname, initials BELLAMY P R 11. Contract Number 15. Distribution statement UNLIMITED Descriptors (or keywords)	g(a) Author 2 12. Period describes a VHF/L rements aimed at the model and the	g(b) Authors 3,4 13. Project continue on separate JHF propagation prediverifying the result trial results were m	1989.10 14. Other Re piece of paper lection model at sof the mode at spot f	47 Inference

Continued of next page

\$60/48

CONTINUED

The program was written on an HP 9000 series model 310 computer using BASIC 5.1. This language has a set of commands which allow direct manipulation of complex values, consequently, translation into another language or version of BASIC not having these facilities will require extra programming.